

PHY 752 Solid State Physics
11-11:50 AM MWF Olin 107

Plan for Lecture 23:

- **Transport phenomena and Fermi liquid theory – Chap. 17 in Marder**
- **Boltzmann equation**
- **Thermoelectric phenomena**
- **Hall effect**

Contains materials from Marder's lecture notes

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9	Wed: 02/04/2015	Chap. 8	Electronic structure, LCAO and tight binding	#9	02/06/2015
10	Fri: 02/06/2015	Chap. 8	Band structure examples	#10	02/09/2015
11	Mon: 02/09/2015	Chap. 9	Electron-electron interactions	#11	02/11/2015
12	Wed: 02/11/2015	Chap. 9	Electron-electron interactions	#12	02/13/2015
13	Fri: 02/13/2015	Chap. 9	Electron-electron interactions	#13	02/16/2015
14	Mon: 02/16/2015	Chap. 10	Electronic structure calculation methods	#14	02/18/2015
15	Wed: 02/18/2015	Chap. 10	Electronic structure calculation methods	#15	02/20/2015
16	Fri: 02/20/2015	Chap. 10	Electronic structure calculation methods	#16	02/23/2015
17	Mon: 02/23/2015	Chap. 10	Electronic structure calculation methods	#17	02/25/2015
18	Wed: 02/25/2015	Chap. 10	Electronic structure calculation methods	#18	02/27/2015
19	Fri: 02/27/2015	Chap. 1-3,7-10	Review, Take-home exam distributed		
	Mon: 03/02/2015	APS Meeting	Take-home exam (no class meeting)		
	Wed: 03/04/2015	APS Meeting	Take-home exam (no class meeting)		
	Fri: 03/06/2015	APS Meeting	Take-home exam (no class meeting)		
	Mon: 03/09/2015	Spring break			
	Wed: 03/11/2015	Spring break			
	Fri: 03/13/2015	Spring break			
20	Mon: 03/16/2015		Review Mid-term exam	#19	03/18/2015
21	Wed: 03/18/2015	Chap. 16	Electron Transport	#20	03/20/2015
22	Fri: 03/20/2015	Chap. 16	Electron Transport	#21	03/23/2015
23	Mon: 03/23/2015	Chap. 17	Electron Transport	#22	03/25/2015

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Using previous results based on wavepacket of Bloch waves with wavevectors near $k_c \rightarrow k$ and spatially centered at $r_c \rightarrow r$.

Effective Hamiltonian with electric and magnetic fields:

$$\mathcal{H}(\vec{r}, \vec{p}) = \mathcal{E}(\vec{p} + \vec{A}e/c) - eV(\vec{r})$$

Energy band: $\mathcal{E}(\mathbf{k})$
 where $\hbar\vec{k} \leftrightarrow \vec{p} + e\vec{A}/c$

Equations of motion

$$\dot{\vec{r}} = \frac{\partial \mathcal{H}}{\partial \vec{p}}, \quad \dot{\vec{p}} = -\frac{\partial \mathcal{H}}{\partial \vec{r}},$$

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Equations of motion continued:

$$\dot{\vec{r}} = \frac{\partial \mathcal{E}}{\partial \hbar \vec{k}} \equiv \vec{v}$$

$$\hbar \dot{\vec{k}} = -e\vec{E} - \frac{e\vec{v}}{c} \times \vec{B},$$

Marder's notation for distribution function: $g_{\vec{r}\vec{k}}(t)$
 Number of electrons in volume $dkd\vec{r}$

$$g_{\vec{r}\vec{k}}(t) d\vec{r} D_{\vec{k}} d\vec{k} = 2 \frac{d\vec{k} d\vec{r}}{(2\pi)^3} g_{\vec{r}\vec{k}}(t).$$

density of states

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Properties of the distribution function:
 Continuity equation:

$$\frac{\partial g}{\partial t} = -\frac{\partial}{\partial \vec{r}} \cdot \dot{\vec{r}} g - \frac{\partial}{\partial \vec{k}} \cdot \dot{\vec{k}} g.$$

$$\frac{\partial g}{\partial t} = -\dot{\vec{r}} \cdot \frac{\partial}{\partial \vec{r}} g - \dot{\vec{k}} \cdot \frac{\partial}{\partial \vec{k}} g$$

additional term due to particle interactions

Boltzmann's equation:

$$\frac{\partial g}{\partial t} = -\dot{\vec{r}} \cdot \frac{\partial}{\partial \vec{r}} g - \dot{\vec{k}} \cdot \frac{\partial}{\partial \vec{k}} g + \left. \frac{dg}{dt} \right|_{\text{coll.}}$$

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Relaxation time approximation to collision term

$$\left. \frac{dg}{dt} \right|_{\text{coll.}} = -\frac{1}{\tau} [g_{\vec{r}\vec{k}} - f_{\vec{r}\vec{k}}]$$

Fermi-Dirac distribution

$$f_{\vec{r}\vec{k}} = \frac{1}{e^{\beta_{\vec{r}}(\mathcal{E}_{\vec{k}} - \mu_{\vec{r}})} + 1}$$

Solution to Boltzmann equation in relaxation time approximation:

$$\frac{dg}{dt} = \frac{\partial g}{\partial t} + \dot{\vec{r}} \cdot \frac{\partial g}{\partial \vec{r}} + \dot{\vec{k}} \cdot \frac{\partial g}{\partial \vec{k}}$$

$$\frac{dg}{dt} = -\frac{g-f}{\tau_{\mathcal{E}}}$$

$$\Rightarrow g_{\vec{r}\vec{k}}(t) = \int_{-\infty}^t dt' f(t') \frac{e^{-(t-t')/\tau_{\mathcal{E}}}}{\tau_{\mathcal{E}}}.$$

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Finding distribution function in relaxation time approximation
 -- continued

$$g_{\vec{r}\vec{k}}(t) = \int_{-\infty}^t dt' f(t') \frac{e^{-(t-t')/\tau_{\mathcal{E}}}}{\tau_{\mathcal{E}}}.$$

Integrating by parts:

$$g_{\vec{r}\vec{k}}(t) = f_{\vec{r}\vec{k}} - \int_{-\infty}^t dt' e^{-(t-t')/\tau_{\mathcal{E}}} \frac{d}{dt'} f(t').$$

$$\frac{df}{dt'} = \left(\vec{r}_{t'} \frac{\partial}{\partial \vec{r}} + \vec{k}_{t'} \frac{\partial}{\partial \vec{k}} \right) f$$

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Finding distribution function in relaxation time approximation
 -- continued

$$f_{\vec{r}\vec{k}} = \frac{1}{e^{\beta_f(\mathcal{E}_{\vec{k}} - \mu_f)} + 1}$$

$$\frac{\partial f}{\partial \vec{r}} = \frac{\partial f}{\partial \mathcal{E}} \left(-\nabla \mu - (\mathcal{E} - \mu) \frac{\nabla T}{T} \right) \quad \frac{\partial f}{\partial \vec{k}} = \frac{\partial f}{\partial \mathcal{E}} \frac{\partial \mathcal{E}}{\partial \vec{k}} = \frac{\partial f}{\partial \mathcal{E}} \hbar \vec{v}$$

$$g_{\vec{r}\vec{k}}(t) = f_{\vec{r}\vec{k}} - \int_{-\infty}^t dt' e^{-(t-t')/\tau_{\mathcal{E}}} \frac{d}{dt'} f(t').$$

$$\frac{df}{dt'} = \left(\vec{r}_{t'} \frac{\partial}{\partial \vec{r}} + \vec{k}_{t'} \frac{\partial}{\partial \vec{k}} \right) f$$

$$g = f - \int_{-\infty}^t dt' e^{-(t-t')/\tau_{\mathcal{E}}} \vec{v}_{\vec{k}} \cdot \left\{ e \vec{E} + \vec{\nabla} \mu + \frac{\mathcal{E}_{\vec{k}} - \mu}{T} \vec{\nabla} T \right\} \frac{\partial f(t')}{\partial \mu}$$

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Finding distribution function in relaxation time approximation
 -- continued

$$g = f - \int_{-\infty}^t dt' e^{-(t-t')/\tau_{\mathcal{E}}} \vec{v}_{\vec{k}} \cdot \left\{ e \vec{E} + \vec{\nabla} \mu + \frac{\mathcal{E}_{\vec{k}} - \mu}{T} \vec{\nabla} T \right\} \frac{\partial f(t')}{\partial \mu}$$

If the relaxation time $\tau_{\mathcal{E}}$ is faster than the other variables, the integral can be approximated as:

$$g = f - \tau_{\mathcal{E}} \vec{v}_{\vec{k}} \cdot \left\{ e \vec{E} + \vec{\nabla} \mu + \frac{\mathcal{E}_{\vec{k}} - \mu}{T} \vec{\nabla} T \right\} \frac{\partial f}{\partial \mu}.$$

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Application to electrical current in the presence of a uniform electric field

$$\vec{j} = \frac{\vec{J}}{V} = -e \int [d\vec{k}] \vec{v}_{\vec{k}} g_{\vec{k}}$$

Recall that $\int [d\vec{k}] \equiv \frac{2}{V} \sum_{\vec{k}} = \frac{2}{(2\pi)^3} \int d\vec{k}$

$$\begin{aligned} \frac{\partial j_{\alpha}}{\partial E_{\beta}} &\equiv \sigma_{\alpha\beta} \\ &= e^2 \int [d\vec{k}] \tau_{\epsilon} v_{\alpha} v_{\beta} \frac{\partial f}{\partial \mu} \end{aligned}$$

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Application to electrical current in the presence of a uniform electric field -- continued

$$\sigma_{\alpha\beta} = e^2 \int [d\vec{k}] \tau_{\epsilon} v_{\alpha} v_{\beta} \frac{\partial f}{\partial \mu}$$

Note that $\frac{\partial f}{\partial \mu} \approx \delta(\mathcal{E} - \mathcal{E}_F)$

$$\sigma_{\alpha\beta} = e^2 \int [d\vec{k}] \tau_{\epsilon} v_{\alpha} v_{\beta} \delta(\mathcal{E} - \mathcal{E}_F)$$

→ Only the Fermi surface contributes to the conductivity

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Application to electrical current in the presence of a uniform electric field -- continued

Alternate expression:

$$\sigma_{\alpha\beta} = e^2 \tau \int [d\vec{k}] f_{\vec{k}} (\mathbf{M}^{-1})_{\alpha\beta}$$

For isotropic system:

$$\sigma = \frac{ne^2\tau}{m^*}$$

where:

$$\frac{1}{m^*} = \frac{1}{3n} \int [d\vec{k}] f_{\vec{k}} \text{Tr}(\mathbf{M}^{-1})$$

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Effects of heat and temperature

For a constant volume process, the first law of thermo says

$$T \frac{\partial S}{\partial t} = \frac{\partial \mathcal{E}}{\partial t} - \mu \frac{\partial N}{\partial t}$$

Define particle current: $\vec{J}_N = N \vec{v}$

Define energy current: $\vec{J}_\mathcal{E} = \mathcal{E} \frac{\vec{J}_N}{N}$

$$\frac{\partial N}{\partial t} + \vec{\nabla} \cdot \vec{J}_N = 0$$

External force acting on system

$$\frac{\partial \mathcal{E}}{\partial t} + \vec{\nabla} \cdot \vec{J}_\mathcal{E} = \vec{F} \cdot \vec{J}_N$$

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Effects of heat and temperature – continued

Rate of entropy production:

$$\dot{S} \equiv \frac{\partial S}{\partial t} + \vec{\nabla} \cdot \left[\frac{\vec{J}_\mathcal{E} - \mu \vec{J}_N}{T} \right]$$

$$= \frac{\vec{F} \cdot \vec{J}_N}{T} - \vec{\nabla} \cdot \left(\frac{\mu}{T} \right) \cdot \vec{J}_N + \vec{\nabla} \cdot \left(\frac{1}{T} \right) \cdot \vec{J}_\mathcal{E}$$

Rate of heat production

$$\dot{Q} \equiv T \frac{\dot{S}}{V} = \left[-e\vec{E} - \vec{\nabla} \mu - \frac{\vec{\nabla} T}{T} \left(\frac{\mathcal{E}}{N} - \mu \right) \right] \cdot \frac{\vec{J}_N}{V}$$

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Effects of heat and temperature – continued

Heat production per wavenumber and per volume:

$$\dot{Q}_{\vec{r}\vec{k}} = \left[-e\vec{E} - \vec{\nabla} \mu - \frac{\vec{\nabla} T}{T} (\mathcal{E}_{\vec{k}} - \mu) \right] \cdot \vec{v}_{\vec{k}} f_{\vec{k}}$$

Connection with Boltzmann distribution in relaxation approximation:

$$g_{\vec{r}\vec{k}} = f_{\vec{r}\vec{k}} + \int_{-\infty}^t dt' e^{-(t-t')/\tau_\mathcal{E}} \dot{Q}(t') \frac{\partial}{\partial \mu} \ln f(t')$$

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Calculation of response coefficients

$$X_\alpha = \sum_\beta L_{\alpha\beta} x_\beta$$

General form of response coefficients:

$$L_{\alpha\beta} = \int [d\vec{k}_i] d\vec{r}_i \int_{-\infty}^t dt' \frac{d\hat{Q}(t)}{dx_\alpha} e^{-(t-t')/\tau_\varepsilon} \left[\frac{\partial}{\partial \mu} \ln f(t') \right] \frac{d\hat{Q}(t')}{dx_\beta}$$

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Responses involving thermal and electrical gradients

Electrochemical force: $\vec{G} = \vec{E} + \frac{\vec{\nabla} \mu}{e}$

Electrochemical flux: $\vec{j} = -e\vec{J}_N/\mathcal{V} = -e \int \frac{d\vec{r}}{\mathcal{V}} \int [d\vec{k}] \vec{v}_{\vec{k}} g_{\vec{k}}$

Thermal force: $\frac{-\vec{\nabla} T}{T}$

Thermal flux: $\vec{j}_Q = (\vec{J}_\varepsilon - \mu\vec{J}_N)/\mathcal{V} = \int \frac{d\vec{r}}{\mathcal{V}} \int [d\vec{k}] (\varepsilon_{\vec{k}} - \mu) \vec{v}_{\vec{k}} g_{\vec{k}}$

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Responses involving thermal and electrical gradients – continued

Linear coefficients: $\vec{j} = \mathbf{L}^{11} \vec{G} + \mathbf{L}^{12} \left(\frac{-\vec{\nabla} T}{T} \right)$

$$\vec{j}_Q = \mathbf{L}^{21} \vec{G} + \mathbf{L}^{22} \left(\frac{-\vec{\nabla} T}{T} \right)$$

Note that these can be calculated from:

$$\mathbf{L}^{11} = \mathcal{L}^{(0)}, \mathbf{L}^{12} = \mathbf{L}^{21} = -\frac{1}{e} \mathcal{L}^{(1)}, \mathbf{L}^{22} = \frac{1}{e^2} \mathcal{L}^{(2)}$$

where $\mathcal{L}_{\alpha\beta}^{(\nu)} = e^2 \int [d\vec{k}] \tau_\varepsilon \frac{\partial f}{\partial \mu} v_{\alpha\nu} v_{\beta\nu} (\varepsilon_{\vec{k}} - \mu)^\nu$.

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Responses involving thermal and electrical gradients – continued

Define: $\sigma_{\alpha\beta}(\mathcal{E}) = \tau_{\mathcal{E}} e^2 \int [d\vec{k}] v_{\alpha} v_{\beta} \delta(\mathcal{E} - \mathcal{E}_{\vec{k}})$

Note that: $\mathcal{L}_{\alpha\beta}^{(\nu)} = \int d\mathcal{E} \frac{\partial f}{\partial \mu} (\mathcal{E} - \mu)^{\nu} \sigma_{\alpha\beta}(\mathcal{E})$.

$$\frac{\partial f}{\partial \mu} \approx \delta(\mathcal{E} - \mathcal{E}_F)$$

$$\mathcal{L}_{\alpha\beta}^{(0)} = \sigma_{\alpha\beta}(\mathcal{E}_F)$$

$$\mathcal{L}_{\alpha\beta}^{(1)} = \frac{\pi^2}{3} (k_B T)^2 \sigma'_{\alpha\beta}(\mathcal{E}_F)$$

$$\mathcal{L}_{\alpha\beta}^{(2)} = \frac{\pi^2}{3} (k_B T)^2 \sigma_{\alpha\beta}(\mathcal{E}_F)$$

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Example: Thermal conductivity

$$\vec{j} = \mathbf{L}^{11} \vec{G} + \mathbf{L}^{12} \left(\frac{-\vec{\nabla} T}{T} \right)$$

$$\vec{j}_Q = \mathbf{L}^{21} \vec{G} + \mathbf{L}^{22} \left(\frac{-\vec{\nabla} T}{T} \right)$$

Consider the case where there is heat flow but no current:

$$\vec{j} = 0 \quad \vec{j}_Q = \kappa \left(-\vec{\nabla} T \right)$$

$$0 = \mathbf{L}^{11} \vec{G} + \mathbf{L}^{12} \left(\frac{-\vec{\nabla} T}{T} \right)$$

$$\vec{G} = (\mathbf{L}^{11})^{-1} \mathbf{L}^{12} \frac{\vec{\nabla} T}{T},$$

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Example: Thermal conductivity -- continued

$$\vec{j}_Q = \left[\mathbf{L}^{21} (\mathbf{L}^{11})^{-1} \mathbf{L}^{12} - \mathbf{L}^{22} \right] \left(\frac{\vec{\nabla} T}{T} \right)$$

$$\Rightarrow \kappa = \frac{\mathbf{L}^{22}}{T} + \mathcal{O} \left(\frac{k_B T}{\mathcal{E}_F} \right)^2$$

$$\Rightarrow \kappa_{\alpha\beta} = \frac{\pi^2}{3} \frac{k_B^2 T}{e^2} \sigma_{\alpha\beta}$$

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Example: Hall effect

Figure 17.3: Geometry of the Hall effect.

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Example: Hall effect -- continued

$$\hbar \dot{\vec{k}} = -e \frac{\vec{v}}{c} \times \vec{B} - e \vec{E}$$

$$\Rightarrow \vec{B} \times \hbar \dot{\vec{k}} + e \vec{B} \times \vec{E} = -e \vec{B} \times \left(\frac{\vec{v}}{c} \times \vec{B} \right) = -\frac{e}{c} \vec{v}_\perp B^2$$

$$\Rightarrow \vec{v}_\perp = -\frac{\hbar c \vec{B} \times \dot{\vec{k}}}{e B^2} - c \frac{\vec{B} \times \vec{E}}{B^2}$$

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Example: Hall effect -- continued

$$g - f = \int_{-\infty}^t dt' e^{-(t-t')/\tau_\varepsilon} \left[\frac{c\hbar \vec{B} \times \dot{\vec{k}}}{e B^2} \right] \cdot e \vec{E} \frac{\partial f}{\partial \mu}$$

$$= \int_{-\infty}^t dt' e^{-(t-t')/\tau_\varepsilon} \frac{c\hbar \dot{\vec{k}}}{B^2} \cdot [\vec{E} \times \vec{B}] \frac{\partial f}{\partial \mu}$$

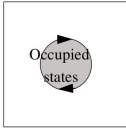
$$= \frac{c\hbar}{B^2} (\vec{k} - \langle \vec{k} \rangle) \cdot [\vec{E} \times \vec{B}] \frac{\partial f}{\partial \mu}$$

$$\langle \vec{k} \rangle = \frac{1}{\tau_\varepsilon} \int_{-\infty}^t dt' e^{-(t-t')/\tau_\varepsilon} \vec{k}(t')$$

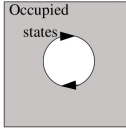
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Example: Hall effect -- continued

Electron like



Hole like



Open orbits

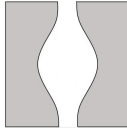


Figure 17.4: Electron-like, hole-like, and open orbits for the Hall effect.

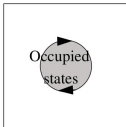
$$\begin{aligned} \vec{j} &= -e \int [d\vec{k}] \vec{v}_k \frac{\partial f}{\partial \mu} \frac{\hbar c}{B^2} \vec{k} \cdot (\vec{E} \times \vec{B}) \\ &= e \int [d\vec{k}] \frac{\partial f}{\partial \hbar \vec{k}} \frac{\hbar c}{B^2} \vec{k} \cdot (\vec{E} \times \vec{B}) \\ &= \left\{ \frac{ec}{B^2} \int [d\vec{k}] \frac{\partial}{\partial \vec{k}} (f \vec{k} \cdot (\vec{E} \times \vec{B})) \right\} - \frac{nec}{B^2} (\vec{E} \times \vec{B}) \end{aligned}$$

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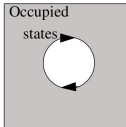


Example: Hall effect -- continued

Electron like



Hole like



$$\vec{j} = -\frac{nec}{B^2} (\vec{E} \times \vec{B}), \quad \vec{j} = \frac{pec}{B^2} (\vec{E} \times \vec{B}),$$

where: $p = \int [d\vec{k}] (1 - f_{\vec{k}})$

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Example: Hall effect -- continued

Hall coefficient:

$$R_H = -\frac{E_x}{B j_y}$$

$$R_H = \begin{cases} -\frac{1}{nec} & \text{for electron carriers} \\ \frac{1}{pec} & \text{for hole carriers} \end{cases}$$

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