

Halliday ♦ Resnick ♦ Walker

FUNDAMENTALS OF PHYSICS
SIXTH EDITION

Selected Solutions

Chapter 13

13.21

13.35

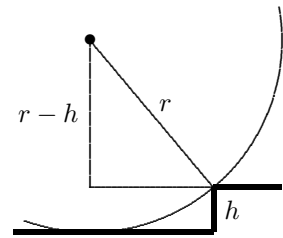
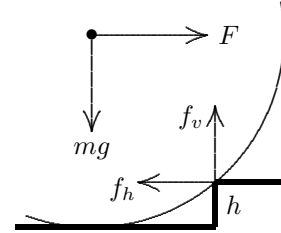
13.39

21.

We consider the wheel as it leaves the lower floor. The floor no longer exerts a force on the wheel, and the only forces acting are the force F applied horizontally at the axle, the force of gravity mg acting vertically at the center of the wheel, and the force of the step corner, shown as the two components f_h and f_v . If the minimum force is applied the wheel does not accelerate, so both the total force and the total torque acting on it are zero.

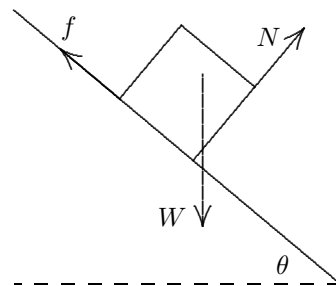
We calculate the torque around the step corner. The second diagram indicates that the distance from the line of F to the corner is $r - h$, where r is the radius of the wheel and h is the height of the step. The distance from the line of mg to the corner is $\sqrt{r^2 + (r - h)^2} = \sqrt{2rh - h^2}$. Thus $F(r - h) - mg\sqrt{2rh - h^2} = 0$. The solution for F is

$$F = \frac{\sqrt{2rh - h^2}}{r - h} mg .$$



35.

The force diagram shown on the right depicts the situation just before the crate tips, when the normal force acts at the front edge. However, it may also be used to calculate the angle for which the crate begins to slide. W is the force of gravity on the crate, N is the normal force of the plane on the crate, and f is the force of friction. We take the x axis to be down the plane and the y axis to be in the direction of the normal force. We assume the acceleration is zero but the crate is on the verge of sliding.



(a) The x and y components of Newton's second law are

$$W \sin \theta - f = 0 \quad \text{and} \quad N - W \cos \theta = 0$$

respectively. The y equation gives $N = W \cos \theta$. Since the crate is about to slide $f = \mu_s N = \mu_s W \cos \theta$, where μ_s is the coefficient of static friction. We substitute into the x equation and find

$$W \sin \theta - \mu_s W \cos \theta = 0 \implies \tan \theta = \mu_s .$$

This leads to $\theta = \tan^{-1} \mu_s = \tan^{-1} 0.60 = 31.0^\circ$.

In developing an expression for the total torque about the center of mass when the crate is about to tip, we find that the normal force and the force of friction act at the front edge. The torque associated with the force of friction tends to turn the crate clockwise and has magnitude fh , where h is the perpendicular distance from the bottom of the crate to the center of gravity. The torque associated with the normal force tends to turn the crate counterclockwise and has magnitude $N\ell/2$, where ℓ is the length of a edge. Since the total torque vanishes, $fh = N\ell/2$. When the crate is about to tip, the acceleration of the center of gravity vanishes, so $f = W \sin \theta$ and $N = W \cos \theta$. Substituting these expressions into the torque equation, we obtain

$$\theta = \tan^{-1} \frac{\ell}{2h} = \tan^{-1} \frac{1.2 \text{ m}}{2(0.90 \text{ m})} = 33.7^\circ .$$

As θ is increased from zero the crate slides before it tips. It starts to slide when $\theta = 31.0^\circ$.

(b) The analysis is the same. The crate begins to slide when $\theta = \tan^{-1} \mu_s = \tan^{-1} 0.70 = 35.0^\circ$ and begins to tip when $\theta = 33.7^\circ$. Thus, it tips first as the angle is increased. Tipping begins at $\theta = 33.7^\circ$.

39. (a) Let F_A and F_B be the forces exerted by the wires on the log and let m be the mass of the log. Since the log is in equilibrium $F_A + F_B - mg = 0$. Information given about the stretching of the wires allows us to find a relationship between F_A and F_B . If wire A originally had a length L_A and stretches by ΔL_A , then $\Delta L_A = F_A L_A / AE$, where A is the cross-sectional area of the wire and E is Young's modulus for steel ($200 \times 10^9 \text{ N/m}^2$). Similarly, $\Delta L_B = F_B L_B / AE$. If ℓ is the amount by which B was originally longer than A then, since they have the same length after the log is attached, $\Delta L_A = \Delta L_B + \ell$. This means

$$\frac{F_A L_A}{AE} = \frac{F_B L_B}{AE} + \ell .$$

We solve for F_B :

$$F_B = \frac{F_A L_A}{L_B} - \frac{AE\ell}{L_B} .$$

We substitute into $F_A + F_B - mg = 0$ and obtain

$$F_A = \frac{mgL_B + AE\ell}{L_A + L_B} .$$

The cross-sectional area of a wire is $A = \pi r^2 = \pi(1.20 \times 10^{-3} \text{ m})^2 = 4.52 \times 10^{-6} \text{ m}^2$. Both L_A and L_B may be taken to be 2.50 m without loss of significance. Thus

$$\begin{aligned} F_A &= \frac{(103 \text{ kg})(9.8 \text{ m/s}^2)(2.50 \text{ m}) + (4.52 \times 10^{-6} \text{ m}^2)(200 \times 10^9 \text{ N/m}^2)(2.0 \times 10^{-3} \text{ m})}{2.50 \text{ m} + 2.50 \text{ m}} \\ &= 866 \text{ N} . \end{aligned}$$

- (b) From the condition $F_A + F_B - mg = 0$, we obtain

$$F_B = mg - F_A = (103 \text{ kg})(9.8 \text{ m/s}^2) - 866 \text{ N} = 143 \text{ N} .$$

- (c) The net torque must also vanish. We place the origin on the surface of the log at a point directly above the center of mass. The force of gravity does not exert a torque about this point. Then, the torque equation becomes $F_A d_A - F_B d_B = 0$, which leads to

$$\frac{d_A}{d_B} = \frac{F_B}{F_A} = \frac{143 \text{ N}}{866 \text{ N}} = 0.165 .$$